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21 April 1997



PRODUCER STATEMENT - DESIGN No. 2937

Issued by: **Graham N. RUNDLE**
to: **GARRY RANKIN**
To be supplied to: **TAURANGA DISTRICT COUNCIL**
in respect of: **ALTERATIONS TO GARAGE**
at: **10 ANCHORAGE GROVE, TAURANGA**

Graham N. RUNDLE Professional Engineer Ltd has been engaged by
TREVOR JONES DESIGN LTD
to provide engineering design services in respect of the requirements of
Clause B1
of the Building Regulations 1992 for those parts of the building work specified in the
accompanying calculations. The design has been prepared in accordance with
B1/VM1 & AS1
of the approved documents issued by the Building Industry Authority and the work
is described on **TREVOR JONES DESIGN LTD**
drawings titled **ALTERATIONS TO GARAGE**
and the specification and other documents according to which the building is proposed
to be constructed.

As an independent design professional covered by current policy of Professional
Indemnity Insurance to a minimum value of \$200,000, I believe on reasonable grounds
that subject to the safe ground bearing pressure being no less than 70 kPa and all
proprietary products meeting the performance requirements, the drawings, specifications
and other documents to which the building is proposed to be constructed comply with the
relevant provisions of the building code.


 24/4/97

Graham N. RUNDLE BE M.IPENZ ERB Registration No. 7733



CALCULATIONS

Page 1

Client: **TREVOR JONES DESIGN LTD**

20 Apr '97

Project: **ALTERATIONS TO GARAGE**

Project No.

2937

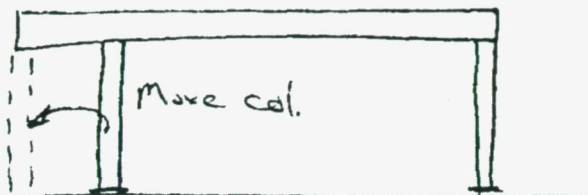
At existing frame at spiral staircase

Loading

Dead. Roof $0.25 \times 3.05 = 0.76 \text{ kN/m}$

Walls $\frac{0.19}{0.25 \times 2} \times 3.05 = 0.58 \text{ kN/m}$

Floor $0.40 \times 3.05 = 1.22 \text{ kN/m}$
 2.53 kN/m



Live Roof $0.25 \times 3.05 = 0.76 \text{ kN/m}$

Floor $1.5 \times 3.05 = 4.58 \text{ kN/m}$
 5.34 kN/m

$$1.2G + 1.6Q \quad M^* = (1.2 \times 2.53 + 1.6 \times 5.34) \times 6.1^2 / 8 = 11.6 \text{ kN-m}$$

$$12 \times 4 \times 16 \text{ RSJ} \quad \delta_{G+Q} = \frac{5}{384} \times \frac{(2.53 + 0.7 \times 5.34) \times 6100^4}{200 \times 10^3 \times 4290 \times 10^4} = 13.2 \text{ mm} \quad \frac{Span}{463}$$

$$f_s = \frac{11.6 \times 10^6}{0.9 \times 280 \times 10^3} = 46 \text{ MPa} \quad \therefore \text{Quite OK.}$$

$$\text{Reaction at new post} = (2.53 + 5.34) \times 6.1 / 2 = 24 \text{ kN}$$

$$\text{Required bearing area for } 70 \text{ kPa} = \frac{24}{70} = 0.34 \text{ m}^2 \quad \frac{600 \times 600}{70}$$

\therefore Move existing column over to end of beam. Fully weld into position

At existing corner of garage

Provide $600 \times 600 \times 200 \text{ per}$
under $-3D16 \text{ var.}$
or 250 \# post hole

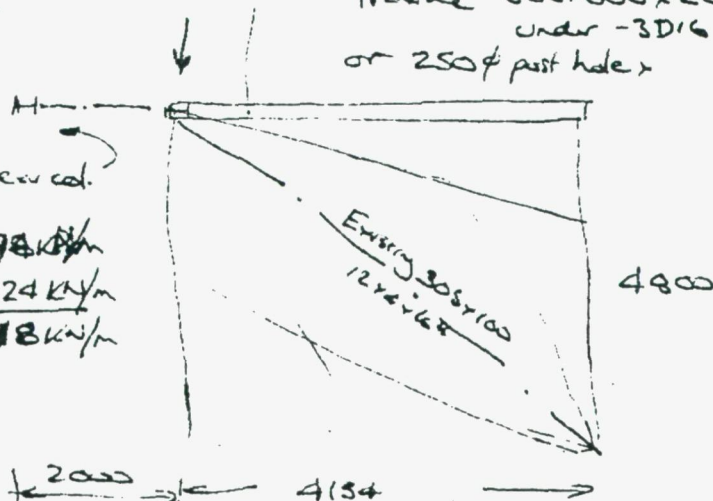
Loading

Pt load from angled beam under deck

Dead Decking $0.40 \text{ kN} \times 4.7 \frac{1}{2} = 1.88 \text{ kN}$
Sill. 0.24 kN/m
 1.48 kN/m

Live $2.0 \times 4.7 \frac{1}{2} = 4.7 \text{ kN/m}$

$$1.2G + 1.6Q \quad P^* = (1.2 \times 1.48 + 1.6 \times 4.7) \times 6.3 \frac{1}{2} = 28.45 \text{ kN}$$





CALCULATIONS

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$$W^*_{\text{Dead}} = (0.25 + 0.19 + 0.40) \times 4.5/2 = 1.86 \text{ kN/m}$$

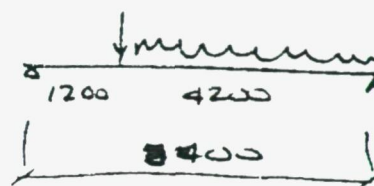
$$S_{\text{ex}} = \frac{0.24}{2.10} \text{ kN/m}$$

$$W^*_{\text{Live}} = (0.25 + 1.5) \times 4.5/2 = 3.93 \text{ kN/m}$$

$$1.2G + 1.6Q \quad W^* = 1.2 \times 2.06 + 1.6 \times 3.93 = 8.81 \text{ kN/m}$$

$$R^*_N = 28.15 \times \frac{4.2}{5.4} + 8.93 \times \frac{4.2 \times 2.1}{5.4}$$

$$= 36.32 \text{ kN} \quad R_s = 24.3 \text{ kN}$$



Max BM @ 2.13 from A.

$$M^* = 36.32 \times 2.13 - 28.15 \times 0.913 - 8.93 \times 0.913/2$$

$$= 47.87 \text{ kN}\cdot\text{m}$$

$$\text{Deflection } \delta_G + \psi_Q \approx \frac{5}{384} \times \frac{(2.11 + 0.7 \times 3.94) \times 5400^4}{200 \times 10^3 \times 42.9 \times 10^6} + \frac{(1.19 + 0.7 \times 4.7) \times 6.3^3}{1200^3 \times 4200^3}$$

$$= 6.28 + 2.57 = 8.85 \text{ mm} \quad \frac{S_{\text{ex}}}{G_0} \therefore \text{OK} \quad 3 \times 200 \times 10^3 \times 42.9 \times 10^6 = 540$$

Support on 250φ post hole piles.

$$\text{Capacity of } 250^{\phi} \text{ pile} = \pi \times 0.25^2/4 \times 1.5 \times 70 + \pi \times 0.25 \times 8.33 \times h$$

$$= 6.54 + 5.15h \quad \therefore \text{NG}$$

For 400φ $Q_u = 13.2 + 10.5 \times h$ \therefore Use 400φ x 1.200 deep.

post hole under each new post.

\therefore Extend frame by welding on extra length of 12" x 4" x 16" RSJ
& relocating post - extend if necessary.
Found on 400φ x 1.200 deep post hole pile.



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Rafters: **12' X 4" X 16# RSJ** Grade: 250

Bending: $\phi M_{sx} = 63.00 \text{ kN-M}$

$\phi M_{sy} = 5.20 \text{ kN-M}$

Load Case: 1.2G & 1.6Q $M_x^* = 47.87 \text{ kN-M}$

$M_y^* = 0 \text{ kN-M}$

For $L_x = 2.100$ $k_t = 1.0$

$k_l = 1.0$

$k_r = 1.0$

$L_{ex} = 2.100$ $\alpha_s = 0.571$

For $\alpha_m = 1.35$

$\phi M_b = 48.59 \text{ kN-M}$ **OK**

Section Properties:

$d = 305 \text{ mm}$

$b_f = 102 \text{ mm}$

$t_f = 6.73 \text{ mm}$

$t_w = 5.59 \text{ mm}$

$d_1 = 3 \text{ mm}$

$A_g = 3039 \text{ mm}^2$

$I_x = 42.9 \times 10^6 \text{ mm}^4$

$Z_x = 280 \times 10^3 \text{ mm}^3$

$S_x = 280 \times 10^3 \text{ mm}^3$

$r_x = 119 \text{ mm}$

$I_y = 1.17 \times 10^6 \text{ mm}^4$

$Z_y = 23.1 \times 10^3 \text{ mm}^3$

$S_y = 23.1 \times 10^3 \text{ mm}^3$

$r_y = 19.6 \text{ mm}$

$J = 38.6 \times 10^3 \text{ mm}^4$

$I_w = 10.4 \times 10^9 \text{ mm}^6$

$f_{ty} = 250 \text{ MPa}$

$k_f = 1$

Compact: **N**

$Z_{ex} = 280 \times 10^3 \text{ mm}^3$

$Z_{ey} = 23.1 \times 10^3 \text{ mm}^3$